

# Absolute Humidity from Relative Humidity

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## Abstract

A set of python functions are described that convert relative humidity (0 – 100%) to absolute humidity (kg of water per kg of dry air), volumetric humidity (g of water per m<sup>3</sup> of air), and dew point (°C) for water-air systems in meteorological temperature and pressure ranges. An implementation using a BME280 pressure and temperature sensor is described.

## 1 Background

Humidity of ambient air is an important factor for human comfort. As of 2021, low-cost humidity measurement electronic modules are often integrated into smartphones, personal wristwatches (see “ABC” or “altitude, barometric, compass” watches), and electric thermometers. The default units of humidity displayed by such devices is often “RH” or “relative humidity”. Relative humidity of air could be described as how much air’s ability to absorb water vapor is occupied. Relative humidity of air, usually expressed as a percentage, is a dimensionless ratio of the current value of the partial pressure of water vapor to its theoretical maximum value. However, this theoretical maximum capacity varies depending on air temperature; for example, if a room in a typical human dwelling is sealed (by closing doors and air vents) and then heated (with a space heater), the relative humidity of the room’s air will fall despite no water vapor leaving the system.

### 1.1 Definitions and Notation

Most equations used in this work use notation used in [2, Sonntag (1994)]. Some equations use notation used in [1, Green (2008)]. All equations are accompanied by variable definitions for clarity. Note that equations from [1, Green (2008)] usually have consistent units while equations from [2, Sonntag (1994)] require careful inspection of assumed units of variables and constants.

### 1.2 Conversion Equations

#### 1.2.1 Sonntag-1990 equation for saturation vapor pressure of water $e_w$

$$\ln(e_w(T)) = -6096.93 T^{-1} + 21.2409642 - 2.711193 \times 10^{-2} T + 1.673952 \times 10^{-5} T^2 + 2.433502 \ln(T) \quad (1)$$

$$173.15 \text{ K} \leq T \leq 373.15 \text{ K} \quad (2)$$

$$s_{\text{rel}} < \pm 0.5\% \quad (-100 \text{ to } -50 \text{ }^\circ\text{C}) \quad (3)$$

$$s_{\text{rel}} < \pm 0.3\% \quad (-50 \text{ to } -0 \text{ }^\circ\text{C}) \quad (4)$$

$$s_{\text{rel}} < \pm 0.005\% \quad (-0 \text{ to } -100 \text{ }^\circ\text{C}) \quad (5)$$

Where:

$e_w$  : saturation vapor pressure (Pa)

$T$  : temperature (K)

$s_{\text{rel}}$  : relative standard deviation

Equation 1 is equation 7 of [2, Sonntag (1994)], “Advancements in the field of hygrometry”. Note that this equation should strictly be multiplied by an enhancement factor  $f$  since the vapor pressure of water predicted by the equation is for pure water vapor (no other gases such as oxygen or nitrogen present). However, according to [1, Green (2008)], the inaccuracy introduced by neglecting  $f$  is “less than 0.5 percent, except at elevated pressures”. Therefore,  $f$  is “usually neglected for engineering calculations”. If  $f$  were to be taken into account, then equations for  $f(P, T)$  in “meteorological temperature and pressure range” are provided in [2, Sonntag (1994)].

Equations 3, 4, and 5 are from [2, Sonntag (1994)] and indicate the different relative standard deviations for  $\ln(e_w(T))$  that apply for different temperature ranges.  $s_{\text{rel}}$  values limit the accuracy of calculations made using  $\ln(e_w(T))$  as input.

### 1.2.2 Saturation vapor pressures of moist air

$$e'_w(t) = f_w(p, t) e_w(t) \quad (6)$$

$$e' = f_w(p, t_d) e_w(t_d) \quad (7)$$

$$e' = f_w(p, t_d) e \quad (8)$$

Where:

- $e'_w(t)$  : saturation vapor pressure of water in moist air
- $f_w(p, t)$  : enhancement factor as a function of  $p$  and  $t$
- $e_w(t)$  : saturation vapor pressure of water (e.g. no O<sub>2</sub> or N<sub>2</sub>)
- $e'$  : vapor pressure of water in moist air
- $e$  : vapor pressure of water in the pure phase
- $p$  : total pressure
- $t$  : temperature

Equations 6 and 7 are equations 18 and 20 of [2, Sonntag (1994)]. Equation 8 is the result of substituting equation 23 into equation 7.

The enhancement factor  $f_w$  is required when taking into account the fact that the vapor pressure of a gas that contains only water molecules is different from the vapor pressure of water molecules that are mixed with other components in a gas mixture.  $e_w$  is strictly the saturation vapor pressure of water in systems where only water is present; introduction of air (i.e. oxygen, nitrogen, etc.) into the system also introduces an error in calculations in which the saturation vapor pressure of the water component of the gas mixture is desired. According to [1, Green (2008)], the correction factor needed to compensate for this error (i.e.  $f_w$ ) is “typically less than 0.5 percent, except at elevated pressures”. For purposes of this article,  $f_w$  will be taken into account; see equation 9.

Equation 7 indicates that the vapor pressure of water in moist air  $e'$  may be calculated as a function of only upon the system’s total air pressure  $p$  and the system’s water dew point temperature  $t_d$ .

Equation 8 is equation 7 but with equation 23 applied. Equation 8 encapsulates the idea that a non-saturated mixture of water vapor and air has a water vapor pressure that is the same as that of the mixture when cooled to its dew point temperature and total pressure is held constant.

### 1.2.3 Enhancement factor $f$

$$f_w(p, t) = 1 + \frac{10^{-4} e_w(t)}{273 + t} \left[ (38 + 173 \exp(-t/43)) \left( 1 - \frac{e_w(t)}{p} \right) + (6.39 + 4.28 \exp(-t/107)) \left( \frac{p}{e_w(t)} - 1 \right) \right] \quad (9)$$

Where:

- $f_w$  : enhancement factor for water
- $p$  : total pressure (hPa)
- $t$  : temperature (°C)
- $e_w$  : saturation vapor pressure with respect to water (hPa)

Equation 9 is equation 22 of [2, Sonntag (1994)]. It is meant to be used with equations 6 and 7.

If  $t$  is neglected, an approximation for  $f_w$  as only a function of pressure can be made. For this, [2, Sonntag (1994)] offers two options:

$$f(p) \cong f_w(p, t) \cong 1.0016 + 3.15 \times 10^{-6} p - \frac{0.074}{p} \quad (10)$$

Where:

$$\begin{aligned} f &: \text{enhancement factor} \\ f_w &: \text{enhancement factor for water} \\ p &: \text{total pressure (hPa)} \end{aligned}$$

Equation 10 is equation 24 in [2, Sonntag (1994)], according to which has a standard deviation of  $< \pm 0.000013$  for the temperature range  $-50$  to  $+70^\circ\text{C}$ .

#### 1.2.4 Definition of relative humidity

$$U_w = \frac{e'}{e'_w(p, t)} \times 100\% \quad (11)$$

Where:

$$\begin{aligned} U_w &: \text{relative humidity (\%)} \\ e' &: \text{vapor pressure of water in an air-water system} \\ e'_w &: \text{saturation vapor pressure of water in an air-water system} \end{aligned}$$

This equation is provided as equation 31 in [2, Sonntag (1994)]. An analogous equation is presented by [1, Green (2008)] on page 12-4 as “RH=100  $p/p_s$ ”; in this context,  $p$  stands for “partial pressure of vapor in a gas-vapor mixture” and  $p_s$  is  $p$  when the system is fully saturated with vapor (i.e. water).

This work will continue to use  $U$  as the symbol for relative humidity.

#### 1.2.5 Interconversion from vapor pressure $p$ to absolute humidity $Y$

$$Y = \frac{p M_v}{(P - p) M_g} \quad (12)$$

Where:

$$\begin{aligned} Y &: \text{absolute humidity} \left( \frac{\text{kg of water}}{\text{kg of dry air}} \right) \\ p &: \text{vapor pressure of vapor (Pa)} \\ P &: \text{total pressure (Pa)} \\ M_v &: \text{molecular weight of vapor} \left( \frac{\text{g}}{\text{mol}} \right) \\ M_g &: \text{molecular weight of gas} \left( \frac{\text{g}}{\text{mol}} \right) \end{aligned}$$

This equation is adapted from an equation in Table 12-2 of [1, Green (2008)] “Interconversion Formulas for a General Gas-Vapor System”. The equation is generalized for systems besides that of air-water. For purposes of this article, water is the vapor and air is the gas.

Equation 12 is analogous to equation 28 of [2, Sonntag (1994)] which is equation 13 below:

$$r = \frac{\varepsilon e'}{p - e'} \quad (13)$$

$$\varepsilon = \frac{M_v}{M_a} = 0.62198 \pm 0.00002 \quad (14)$$

Where:

$$\begin{aligned} r &: \text{mixing ratio of moist air} \left( \frac{\text{kg water vapor}}{\text{kg dry air}} \right) \\ \varepsilon &: \text{ratio of molar mass of dry air and water vapor} \\ e' &: \text{vapor pressure of water (Pa)} \\ p &: \text{total pressure (Pa)} \\ M_v &: \text{molar mass of water vapor} \left( \frac{\text{kg}}{\text{mol}} \right) \\ M_a &: \text{molar mass of dry air} \left( \frac{\text{kg}}{\text{mol}} \right) \end{aligned}$$

Equation 14 is equation 6 of [2, Sonntag (1994)].

### 1.2.6 Interconversion from volumetric humidity $Y_v$ to absolute humidity $Y$

$$Y = \frac{M_v}{M_g \left( \frac{PM_v}{Y_v RT} - 1 \right)} \quad (15)$$

$$Y_{\text{real}} = \frac{M_v}{M_g \left( \frac{PM_v}{Y_v Z RT} - 1 \right)} \quad (16)$$

$$R = 8.314\,462\,618\,153\,54 \frac{\text{J}}{\text{mol}\cdot\text{K}} \quad (17)$$

$$Y_v = C_2 \cdot d_v \quad (18)$$

$$C_2 = \left( \frac{\text{g}}{\text{m}^3} \right) \left( \frac{\text{kg}}{1000 \text{ g}} \right) \quad (19)$$

$$= 10^{-3} \left( \frac{\text{kg}/\text{m}^3}{\text{g}/\text{m}^3} \right) \quad (20)$$

Where:

$$Y : \text{absolute humidity, ideal gas} \left( \frac{\text{kg of water}}{\text{kg of dry air}} \right)$$

$$Y_{\text{real}} : \text{absolute humidity} \left( \frac{\text{kg of water}}{\text{kg of dry air}} \right)$$

$$Y_v : \text{volumetric humidity} \left( \frac{\text{kg of water}}{\text{m}^3 \text{ of dry air}} \right)$$

$$P : \text{total pressure (Pa)}$$

$$M_v : \text{molecular weight of vapor} \left( \frac{\text{g}}{\text{mol}} \right)$$

$$M_g : \text{molecular weight of gas} \left( \frac{\text{g}}{\text{mol}} \right)$$

$$R : \text{gas constant} \left( \frac{\text{J}}{\text{mol}\cdot\text{K}} \right)$$

$$T : \text{temperature (K)}$$

$$d_v : \text{volumetric humidity} \left( \frac{\text{g}}{\text{m}^3} \right)$$

$$C_2 : \text{unit consistency constant} \left( \frac{\text{kg}/\text{m}^3}{\text{g}/\text{m}^3} \right)$$

Equation 15 is from [1, Green (2008)] that interconverts volumetric humidity  $Y_v$  (mass water per volume air) to absolute humidity  $Y$  (mass water per mass dry air). Equation 15 is adapted into equation 16 by reintroducing compressibility  $Z$  since the equation 15 was derived assuming an ideal gas while, in contrast, this work is taking compressibility into account. Equation 18 permits use of the volumetric humidity  $d_v$  calculated by equation 32. Equation 17 defines the universal gas constant  $R$  according to the 2019 redefinition of SI base units.

### 1.2.7 Derivation of dewpoint temperature $t_d$ from $p$

$$t_d = 13.715 y + 8.4262 \times 10^{-1} y^2 + 1.9048 \times 10^{-2} y^3 + 7.8158 \times 10^{-3} y^4 \quad (21)$$

$$y = \ln \left( \frac{e}{611.213 \text{ Pa}} \right) \quad (22)$$

$$e = e_w(t_d) \quad (23)$$

$$T_d = 273.15 + t_d \quad (24)$$

Where:

- $t_d$  : dew point or “saturation temperature” (°C)
- $T_d$  : dew point or “saturation temperature” (K)
- $e_w(t_d)$  : saturation vapor pressure of water at the dew point (Pa)
- $e$  : vapor pressure of water (Pa)
- $y$  : substitution variable used to simplify Equation 21.

Equations 21 and 22 are adapted from equations 10 and 9 in [2, Sonntag (1994)] respectively. Equation 23 is part of equation 9 of [2, Sonntag (1994)].

To explain, if an air-water gas system is cooled at constant pressure to the dew point temperature  $t_d$ , then liquid water will begin to condense from the gas. Equations 21 and 22 model the relationship between  $t_d$  and  $e$ ; if one is known then the other must have a certain value.

### 1.2.8 Compressibility factor for dry air

$$Z_a \cong 1 - (70 - t) p \times 10^{-8} \quad (25)$$

Where:

- $Z_a$  : compressibility for dry air (-)
- $t$  : temperature (°C)
- $p$  : total pressure (hPa)

Equation 25 is taken from equation 3 in [2, Sonntag (1994)] which also indicates that “ $Z$  is very near to  $Z_a$ ”, implying the equation may be used in case actual values for the actual compressibility of moist air  $Z$  are unavailable. Extremely accurate values of  $Z$  are typically not available since  $Z$  is a function of the mass composition of the gas mixture as well as pressure and temperature; variations in the water content of an air-water mixture changes  $Z$  slightly.

Compressibility  $Z$  is required to calculate the volumetric humidity  $d_{vw}$  in equations 26 and 27. For the purposes of this article, equation 25, which is just a function of  $t$  and  $p$ , will be used to estimate  $Z$ .

### 1.2.9 Saturation value of volumetric humidity $d_{vw}$

$$d_{vw} = \frac{f_w(p, T) e_w(T) \times 10^5}{Z R_v T} \quad (26)$$

$$d_{vw} = \frac{C_1 f_w(p, T) e_w(T)}{Z R_v T} \quad (27)$$

$$C_1 = \left( \frac{100 \text{ Pa}}{\text{hPa}} \right) \left( \frac{1}{\text{Pa}} \cdot \frac{\text{N}}{\text{m}^2} \right) \left( \frac{1}{\text{N}} \cdot \frac{\text{kg} \cdot \text{m}}{\text{s}^2} \right) \left( \frac{\text{J}}{1} \cdot \frac{\text{s}^2}{\text{kg} \cdot \text{m}^2} \right) \left( \frac{1000 \text{ g}}{\text{kg}} \right) \quad (28)$$

$$= 10^5 \frac{\frac{\text{g}}{\text{m}^3}}{\frac{1}{\text{hPa}} \cdot \frac{\text{J}}{\text{kg} \cdot \text{K}} \cdot \frac{\text{K}}{1}} \quad (29)$$

$$R_v = \frac{R}{M_v} = (461.525 \pm 0.013) \frac{\text{J}}{\text{kg} \cdot \text{K}} \quad (30)$$

Where:

- $d_{vw}$  : saturation value of volumetric humidity for water-saturated system  $\left( \frac{\text{g}}{\text{m}^3} \right)$
- $f_w$  : enhancement factor as a function of  $p$  and  $T$  for water-saturated system (-)
- $e_w$  : saturation vapor pressure of water for water-saturated system (hPa)
- $Z$  : compressibility factor for moist air (-)
- $R$  : molar gas constant  $\left( \frac{\text{J}}{\text{mol} \cdot \text{K}} \right)$
- $R_v$  : specific gas constant for water vapor  $\left( \frac{\text{J}}{\text{kg} \cdot \text{K}} \right)$

$$\begin{aligned}
M_v &: \text{molar mass of water vapor} \left( \frac{\text{kg}}{\text{mol}} \right) \\
T &: \text{temperature (K)} \\
p &: \text{total pressure (Pa)} \\
C_1 &: \text{unit consistency constant} \left( \frac{\frac{\text{g}}{\text{m}^3}}{\frac{1}{\text{hPa}} \cdot \frac{\text{J}}{\text{kg} \cdot \text{K}} \cdot \frac{\text{K}}{1}} \right)
\end{aligned}$$

Equation 26 is taken from equation 26 of [2, Sonntag (1994)]. In that work,  $d_{vw}$  is defined as “the saturation value of the absolute humidity with respect to water” with units “ $\text{g}/\text{m}^3$ ” for temperatures up to  $100^\circ\text{C}$ . This work will instead use the term “volumetric humidity” while reserving the term “absolute humidity” for the quantity  $\frac{\text{mass of water}}{\text{mass of dry air}}$ . Equation 30 is equation 2 of [2, Sonntag (1994)] where the uncertainty is “the standard deviation”. Although more precise values for  $R$  and  $M_v$  may be used to calculate  $R_v$ , this work will use the definition given in [2, Sonntag (1994)] for convenience.  $C_1$  is a unit consistency constant used in this work to clarify the units of the  $\times 10^5$  factor so related equations can be made consistent.

### 1.2.10 Volumetric humidity $d_v$

$$d_v = \frac{C_1 f_w(p, T_d) e_w(T_d)}{Z R_v T} \quad (31)$$

$$d_v = \frac{C_1 e'}{Z R_v T} \quad (32)$$

Where:

$$\begin{aligned}
d_v &: \text{volumetric humidity} \left( \frac{\text{g}}{\text{m}^3} \right) \\
C_1 &: \text{unit consistency constant} \left( \frac{\frac{\text{g}}{\text{m}^3}}{\frac{1}{\text{hPa}} \cdot \frac{\text{J}}{\text{kg} \cdot \text{K}} \cdot \frac{\text{K}}{1}} \right). \text{ See equation 29.} \\
f_w &: \text{enhancement factor as a function of } p \text{ and } T \text{ for water-saturated system } (-) \\
T &: \text{temperature (K)} \\
T_d &: \text{dew point temperature (K)} \\
p &: \text{total pressure (Pa)} \\
e_w &: \text{saturation vapor pressure of water for water-saturated system (hPa)} \\
e' &: \text{vapor pressure of water in moist air mixture (hPa)} \\
Z &: \text{compressibility factor for moist air } (-) \\
R_v &: \text{specific gas constant for water vapor} \left( \frac{\text{J}}{\text{kg} \cdot \text{K}} \right). \text{ See equation 30.}
\end{aligned}$$

Equations 31 and 32 are adapted from equations 20, 26, and 32 of [2, Sonntag (1994)] and describe the volumetric humidity  $d_v$  ( $\frac{\text{mass of water vapor}}{\text{volume of moist air}}$ ). It is analogous to the interconversion formula in Table 12-2 of [1, Green (2008)] for converting from vapor pressure  $p$  to volumetric humidity  $Y_v$  in equation 33 below:

$$Y_v = \frac{M_v p}{R T} \quad (33)$$

Where:

$$\begin{aligned}
Y_v &: \text{volumetric humidity} \\
M_v &: \text{molar mass of vapor (e.g. water)} \\
p &: \text{vapor pressure (e.g. water)} \\
R &: \text{universal gas constant} \\
T &: \text{temperature}
\end{aligned}$$

Note that equations such as 33 from [1, Green (2008)] do not take enhancement factors into account. For reference,  $d_v$  is related to the definitions for absolute humidity  $Y$  and volumetric humidity  $Y_v$  by equations 15 and 18 respectively.

### 1.2.11 Conversion between Celsius and Kelvin

$$T = 273.15 + t \quad (34)$$

Where:

- $T$  : temperature (K)
- $t$  : temperature ( $^{\circ}\text{C}$ )

## 2 Methodology

Create a set of python functions that each take the inputs of temperature  $T$  (K), total air pressure  $P$  (Pa), and relative humidity  $U_w$  (%) in order to each produce a single output of either absolute humidity  $Y$  ( $\frac{\text{kg of water}}{\text{kg of dry air}}$ ), volumetric humidity ( $\frac{\text{g of water}}{\text{m}^3 \text{ of air}}$ ), or dew point  $t_d$  ( $^{\circ}\text{C}$ ).

### 2.1 Calculation explanations

#### 2.1.1 Absolute humidity $r$

1. Calculate  $e_w(T)$ , the saturation vapor pressure of water in a pure phase, by solving equation 1 for  $e_w$ . The required input is the given temperature  $T$ .
2. Calculate  $f_w(P, T)$ , the enhancement factor for water, by solving equation 9 for  $f_w(P, T)$ . The required input variables are the given pressure  $P$  and given temperature  $T$ . Apply equation 34 to convert between  $T$  (K) and  $t$  ( $^{\circ}\text{C}$ ). Note that the value of  $e_w(T)$  is already calculated in a previous step.
3. Calculate  $e'_w(P, T)$ , the saturation vapor pressure of water in an air-water mixture, by solving equation 6 for  $e'_w(P, T)$ . The required input variables will be  $f_w$  and  $e_w$ . Apply equation 34 to convert between  $T$  (K) and  $t$  ( $^{\circ}\text{C}$ ).
4. Calculate  $e'$ , the vapor pressure of water in air, by solving equation 11 for  $e'$ . The required input variables are  $e'_w$  and the given relative humidity  $U_w$ .
5. Calculate  $r$ , the absolute humidity ( $\frac{\text{kg water vapor}}{\text{kg dry air}}$ ), by solving equation 13 for  $r$ . The required input variables are vapor pressure of water in air  $e'$  and the given total air pressure  $P$ .

#### 2.1.2 Volumetric humidity $Y_v$

1. Perform the steps in 2.1.1 to calculate the vapor pressure of water in air  $e'$  from the given relative humidity  $U_w$ .
2. Calculate  $Z$ , the compressibility constant of moist air, by approximating it with the compressibility constant for dry air  $Z_a$ , and solving equation 25 for  $Z_a$ .
3. Calculate  $d_v$ , the volumetric humidity ( $\frac{\text{g water vapor}}{\text{m}^3 \text{ moist air}}$ ), by solving equation 32 for  $d_v$ . The required input variables are  $e'$ ,  $T$ , and  $Z$ .
4. Calculate  $Y_v$ , the volumetric humidity ( $\frac{\text{kg water vapor}}{\text{m}^3 \text{ moist air}}$ ), by solving equation 18 for  $Y_v$ . The required input variable is  $d_v$ .

#### 2.1.3 Dew point temperature $t_d$

1. Perform the steps in 2.1.1 to calculate the vapor pressure of water in air  $e'$  from the given relative humidity  $U_w$ .

2. Calculate  $f_w(P, t_d)$ , the enhancement factor for water, by solving equation 9 for  $f_w(P, t_d)$ . The required input variables are the given pressure  $P$  and temperature  $t_d$ . Apply equation 34 to convert between  $T_d$  and  $t_d$ . In the first iteration  $t_d$  is not available since  $f_w(p, t_d)$  is a function of  $t_d$ . Therefore, for the first iteration, use equation 10 to set  $f_w = f(P)$  where  $f$  is an approximation for meteorological conditions that is only a function of pressure. Use subsequent iterations to calculate more accurate values for  $t_d$ .
3. Calculate  $e$ , the vapor pressure of water in the pure phase, by solving equation 8 for  $e$ . The required input variables are  $f_w$  and  $e'$ .
4. Calculate  $y$ , an intermediate dew point calculation variable, by solving equation 22 for  $y$ . The required input variable is  $e$ .
5. Calculate  $t_d$ , the dew point temperature in °C, by solving equation 21 for  $t_d$ . The required input variable is  $y$ . Repeat the calculation steps until adequate convergence for  $t_d$  between iterations is reached.

## 2.2 Python implementation

A PYTHON package `convert/humidity.py` and an accompanying test script `test.py` have been prepared that calculate absolute humidity, volumetric humidity, and dew point temperature. The respective functions defined in are `rel_to_abs`, `rel_to_dpt`, and `rel_to_vol`. A compressed file containing these files is available at:

<https://reboil.com/res/2021/exe/20211002..convert-humidity-snapshot.zip>

The functions have been tested by installing them into a branch of the PIMORONI software published for use with their ENVIRO sensor product which runs on a RASPBERRY PI. The GIT branch of the software is named `master-bk` and is available at:

<https://zdv2.bktei.com/gitweb/EVA-2020-02-2.git>

The original GIT repository is available at:

<https://github.com/pimoroni/enviropius-python.git>

The PIMORONI software contains example PYTHON code for communicating with sensors installed on the ENVIRO sensor such as the BME280. The absolute humidity and dew point temperature functions have been tested as of 2021-10-02.

## Bibliography

- [1] Robert H. Perry and Don W. Green. *Perry's chemical engineers' handbook (8th)*. McGraw-Hill, New York, 8th edition, 2008.
- [2] D. Sonntag. Advancements in the field of hygrometry. *Meteorologische Zeitschrift*, 3(2):51–66, 05 1994.